

# Dynamics of a hysteretic relay oscillator with periodic forcing

Tamás Kalmár-Nagy, Pankaj Wahi, Abhishek Halder

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## Abstract

The dynamics of a hysteretic relay oscillator with simple harmonic forcing is studied in this paper. Even though there are no bounded solutions in the absence of forcing, periodic excitation gives rise to more complex responses including periodic, quasiperiodic and chaotic behavior. A Poincaré map is introduced to facilitate mathematical analysis. Families of period-one solutions are determined as fixed points of the Poincaré map. These represent coexisting subharmonic responses. Conditions on the amplitude and frequency of the forcing for the existence of periodic solutions have been obtained. Linear stability analysis reveals that these solutions can be classified as centers or saddles. The presence of higher periodic, quasiperiodic motions together with homoclinic and heteroclinic tangles imply the existence of chaotic solutions.

## 1 Introduction

Over the past decades, relay systems with hysteresis attracted increasing attention. This class of nonlinear systems have found applications in a wide range of engineering problems including voltage regulators, DC motors, and servomechanisms [1, 2, 3, 4, 5, 6, 7]. Relays, in general, have two output branches and the output of a relay jumps discontinuously whenever the input exceeds a certain critical value as shown in Fig. 1. For an ideal relay, there is a single critical value for which the output is discontinuous while for a relay with hysteresis, there are two such critical input values as shown in Fig. 1.

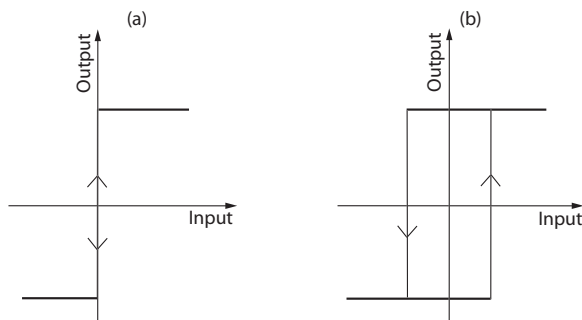


Figure 1: Input-output characteristics of (a) an ideal relay and (b) a relay with hysteresis.

Andronov [2] and Åström [7] studied the existence and stability of period-one solutions (i.e., solutions having exactly two relay switchings per period). Gonçalves *et al.* [8, 9] presented a global analysis of relay systems using Lyapunov functions. Johansson *et al.* and di Bernardo *et al.* extensively studied different aspects of feedback systems with ideal relays (see [10, 11, 12] and references therein). Periodic solutions in a relay system with square-wave excitation was considered by Varigonda and Georgiou [3], while Fleishman [13] focused on periodic response under sinusoidal forcing. A related class of nonlinear systems involve relay operators with delays in the input. Barton *et al.* [14], Fridman *et al.* [15], and Norbury and Wilson [16] considered first order delayed relay systems while Bayer and Heiden [17], Sieber [18], Barton *et al.* [19] and Colombo *et al.* [20] studied second order systems. These studies include periodic solutions, their bifurcations as well as chaotic solutions in these systems with or without forcing.

Hysteretic relay operators are also used in modeling complex hysteresis in materials where they are commonly known as the elementary Preisach operators [21, 22]. However, studies on the response of hysteretic systems modeled using relay operators [23, 24] almost always neglect the dynamics of the relay operators.

Relay systems belong to the general class of piecewise smooth dynamical systems. Other systems belonging to this class include systems with play or backlash [25], systems with friction [26, 27, 28, 29, 30], systems with impacts [26, 27, 28, 30, 31, 32, 33, 34, 35], and other hybrid systems [36, 37, 38, 39]. Leine and van Campen [26] provide an overview and examples of bifurcation phenomena in such non-smooth dynamical systems. In particular, the relay system considered in this study is a piecewise linear system which is similar to the much studied repeated impact of a ball with a sinusoidally vibrating table [31, 40, 41, 42, 43, 44, 45] and its Hamiltonian analog studied in relevance to particle physics [46, 47, 48]. Further, the equation studied in this paper can also be taken as a simple model for automotive suspension with magneto-rheological (MR) damper [49] under periodic forcing.

In this paper, we study the dynamics of a hysteretic relay operator under periodic excitation. It is shown that in this system, a rich variety of dynamic responses ranging from periodic to chaotic solutions exist. We obtain conditions on the parameters, i.e., amplitude and frequency of the forcing for which bounded solutions can exist. To facilitate the analysis, we introduce a 2D Poincaré map. Fixed points of the Poincaré map correspond to periodic solutions of the system. There are two families of period-one solutions corresponding to two families of fixed points of the Poincaré map. On the Poincaré plane, one family of fixed points corresponds to centers while the other corresponds to saddles. There are invariant curves around the centers on the Poincaré plane which correspond to quasiperiodic solutions. The presence of homoclinic tangles has been shown numerically. This indicates the existence of chaotic solutions. As the parameters are varied, the centers and the saddles merge in a saddle-center bifurcation [50, 51]. For these parameter values, there is a single family of non-hyperbolic fixed points corresponding to a single family of period-one solutions with no other bounded solutions.

## 2 Mathematical model of the relay oscillator

The equation studied in this work is

$$\ddot{x}(t) + F[x(t)] = A \cos(\omega t + \phi), \quad A \geq 0, \omega > 0, \phi \in (-\pi, \pi]. \quad (1)$$

Where  $A$ ,  $\omega$ , and  $\phi$  are the amplitude, frequency, and phase of the forcing, respectively. The hysteretic relay operator  $F[x(t)]$  (shown in Fig. 2) is defined as

$$F[x(t)] = \begin{cases} -1, & x(t) \leq 0 \\ e, & 0 < x(t) < 1 \\ 1, & x(t) \geq 1 \end{cases} \quad (2)$$

where  $e$  is  $-1$  or  $1$  depending on the initial conditions and the time history of the solution, i.e., whether the solution enters the hysteretic region  $0 < x(t) < 1$  from the left or right. When  $F[x(t)] = \mp 1$ , the evolution of the

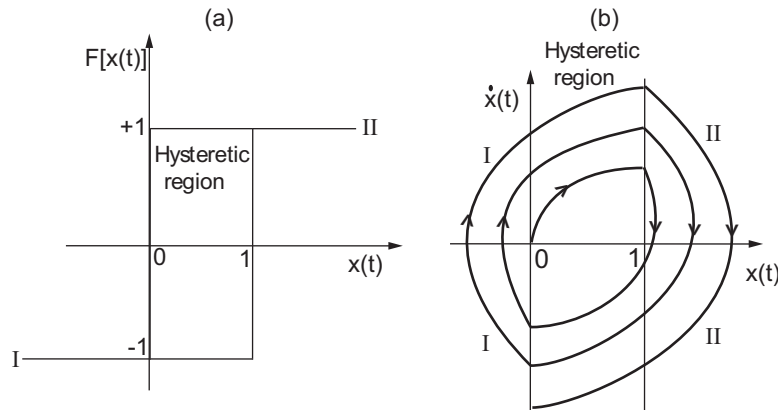


Figure 2: (a) The relay operator with hysteresis. (b) Phase portrait of (1) for  $A=0$ . Initial conditions are  $x(0) = 0$  and  $\dot{x}(0) = 0$ .

dynamical system is described by

$$(I) \quad \ddot{x}_I(t) - 1 = A \cos(\omega t + \phi_I), \quad (3)$$

$$(II) \quad \ddot{x}_{II}(t) + 1 = A \cos(\omega t + \phi_{II}), \quad (4)$$

where the subscripts are used to differentiate between the two subsystems. The complete description of the system also requires initial conditions. Without loss of generality, these initial conditions can be specified as

$$F[x(0)] = -1, \quad x_I(0) = 0, \quad \dot{x}_I(0) = v_I. \quad (5)$$

Figure 2(b) shows the phase portrait in  $x(t)$  and  $\dot{x}(t)$  for the free response of the system (i.e.,  $A = 0$ , see section 4). The dynamics switches between the subsystems when the solution trajectories intersect  $x_I(t) = 1$  from the left, i.e.,  $\dot{x}_I(t) \geq 0$  or  $x_{II}(t) = 0$  from the right, i.e.,  $\dot{x}_{II}(t) \leq 0$ .

To make the analysis simpler, time is reset when transition occurs between subsystems. To account for this artificial time-shift, the phase of the forcing is 'updated' at the switchings. Therefore, the evolution of the dynamics is completely specified by

$$\ddot{x}_I(t) - 1 = A \cos(\omega t + \phi_I), \quad x_I(0) = 0, \dot{x}_I(0) = v_I, \quad t \in [0, t_I] \quad (6)$$

$$\ddot{x}_{II}(t) + 1 = A \cos(\omega t + \phi_{II}), \quad x_{II}(0) = 1, \dot{x}_{II}(0) = v_{II}, \quad t \in [0, t_{II}]. \quad (7)$$

Here  $t_I$  and  $t_{II}$  are the switching times defined implicitly by  $x_I(t_I) = 1$  and  $x_{II}(t_{II}) = 0$ , respectively.

### 3 The phase space and solutions

Figure 3(a) depicts the evolution of solution trajectories in  $x(t)$ ,  $\dot{x}(t)$  and  $F[x(t)]$ . Time  $t$  is introduced as another

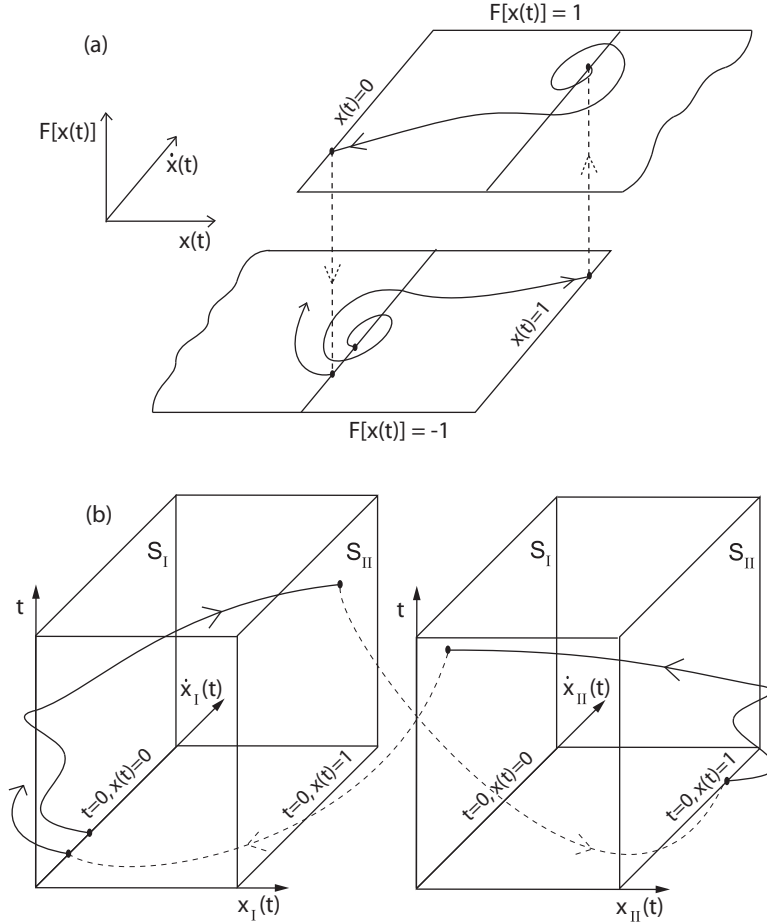


Figure 3: (a) Phase space of (1) in  $x(t)$ ,  $\dot{x}(t)$  and  $F[x(t)]$ . (b) Extended phase space  $(x_I(t), \dot{x}_I(t), t) \cup (x_{II}(t), \dot{x}_{II}(t), t)$

state variable resulting in an extended phase space [25, 31]. Clearly  $x_I(t) \in X_I = (-\infty, -1]$  and  $x_{II}(t) \in X_{II} = [0, \infty)$ . Also,  $\dot{x}_I(t), \dot{x}_{II}(t) \in \mathbb{R}$  and  $t \in \mathbb{R}^+$ . The extended phase space is therefore  $X_I \times \mathbb{R} \times \mathbb{R}^+ \cup X_{II} \times \mathbb{R} \times \mathbb{R}^+$ . This space is a proper subset of  $\mathbb{R}^3 \times \{-1, 1\}$ , where the discrete set  $\{-1, 1\}$  is simply the range of  $F[x(t)]$ .

It is again emphasized in Fig. 3 that the system consists of two distinct subsystems, viz. subsystem  $I$  and subsystem  $II$ . The dynamics of subsystem  $I$  switches to that of subsystem  $II$  when the solution trajectories intersect the surface  $S_{II} = \{(\dot{x}(t), t) | x(t) = 1, \dot{x}(t) \geq 0\}$  and from subsystem  $II$  to subsystem  $I$  when they intersect the plane  $S_I = \{(\dot{x}(t), t) | x(t) = 0, \dot{x}(t) \leq 0\}$  as demonstrated in Fig. 3(b).

Having described the structure of the phase space, we now turn our attention to the solutions. The solution of subsystem  $I$  can be written in closed form as

$$x_I(t) = \frac{1}{2}t^2 + \left(v_I - \frac{A}{\omega} \sin(\phi_I)\right)t + \frac{A}{\omega^2} \cos(\phi_I) - \frac{A}{\omega^2} \cos(\omega t + \phi_I), \quad (8)$$

$$\dot{x}_I(t) = t + v_I - \frac{A}{\omega} \sin(\phi_I) + \frac{A}{\omega} \sin(\omega t + \phi_I). \quad (9)$$

Similarly, the solution of subsystem  $II$  is

$$x_{II}(t) = 1 - \frac{1}{2}t^2 + \left(v_{II} - \frac{A}{\omega} \sin(\phi_{II})\right)t + \frac{A}{\omega^2} \cos(\phi_{II}) - \frac{A}{\omega^2} \cos(\omega t + \phi_{II}), \quad (10)$$

$$\dot{x}_{II}(t) = -t + v_{II} - \frac{A}{\omega} \sin(\phi_{II}) + \frac{A}{\omega} \sin(\omega t + \phi_{II}). \quad (11)$$

Note that the transformation  $(v_I, \phi_I) \rightarrow (-v_{II}, \phi_{II} + \pi)$  in Eqs. (8) and (9) is equivalent to

$$(x_I(t), \dot{x}_I(t)) \rightarrow (1 - x_{II}(t), -\dot{x}_{II}(t)), \quad (12)$$

and the substitution  $(v_{II}, \phi_{II}) \rightarrow (-v_I, \phi_I + \pi)$  in Eqs. (10) and (11) leads to

$$(x_{II}(t), \dot{x}_{II}(t)) \rightarrow (1 - x_I(t), -\dot{x}_I(t)). \quad (13)$$

Therefore a solution of one subsystem with an initial velocity  $v$  and initial phase of the forcing  $\phi$  also represents solution trajectories of the other subsystem with the corresponding initial velocity  $-v$  and initial phase  $\phi + \pi$ . As a consequence, solutions appear in pairs, i.e. if  $(x(t), \dot{x}(t))$  is a solution of Eq. (1), then so is  $(1 - x(t), -\dot{x}(t))$ . This motivates the introduction of the 'shift map'

$$\Psi \begin{pmatrix} v \\ \phi \end{pmatrix} = \begin{pmatrix} -1 & 0 \\ 0 & 1 \end{pmatrix} \begin{pmatrix} v \\ \phi \end{pmatrix} + \begin{pmatrix} 0 \\ \pi \end{pmatrix}. \quad (14)$$

which maps solutions of subsystem  $I$  into those of subsystem  $II$ . This map will be utilized in Section 6 during the construction of the Poincaré map.

Having established some properties of the solutions, we proceed with our analysis of the model. First, the free response of the model is discussed.

## 4 Free response

In this section, we show that in the absence of forcing, i.e.,  $A = 0$ , all solutions of the system are unbounded. The system is now given by

$$\ddot{x}(t) + F[x(t)] = 0. \quad (15)$$

The solution of the subsystems  $I$  and  $II$  for this case becomes

$$x_I(t) = \frac{1}{2}t^2 + v_I t \quad (16)$$

$$\dot{x}_I(t) = t + v_I, \quad (17)$$

and

$$x_{II}(t) = 1 - \frac{1}{2}t^2 + v_{II} t \quad (18)$$

$$\dot{x}_{II}(t) = -t + v_{II}. \quad (19)$$

When  $x_I(t_I) = 1$ , the system switches from subsystem  $I$  to subsystem  $II$ . The equation determining the switching time  $t_I$  is therefore

$$\frac{1}{2}t_I^2 + v_I t_I - 1 = 0, \quad (20)$$

which can be solved in closed form to give (for  $t_I > 0$ )

$$t_I = -v_I + \sqrt{v_I^2 + 2}. \quad (21)$$

Substituting  $t_I$  in Eq. (17), we get the velocity at the switching as

$$\dot{x}_I(t_I) = -v_I + \sqrt{v_I^2 + 2} + v_I = \sqrt{v_I^2 + 2}.$$

The initial velocity for the subsystem  $II$  is  $\dot{x}_{II}(0) = v_{II} = \dot{x}_I(t_I)$ . Substituting  $v_{II} = \sqrt{v_I^2 + 2}$  in Eq. (18), the solution  $x_{II}(t)$  is given by

$$x_{II}(t) = 1 - \frac{1}{2}t^2 + \sqrt{v_I^2 + 2}t. \quad (22)$$

The switch from subsystem  $II$  to subsystem  $I$  occurs when  $x_{II}(t_{II}) = 0$ . This yields

$$1 - \frac{1}{2}t_{II}^2 + \sqrt{v_I^2 + 2}t_{II} = 0. \quad (23)$$

The above equation can again be solved in closed form (for  $t_{II} > 0$ ) to give

$$t_{II} = \sqrt{v_I^2 + 2} + \sqrt{v_I^2 + 4}. \quad (24)$$

Substituting  $t_{II}$  from Eq. (24) into Eq. (19), we get

$$v_{II}(t_{II}) = -\sqrt{v_I^2 + 4}. \quad (25)$$

which is also the next initial velocity for subsystem  $I$ , i.e.  $\dot{x}_I(0) = v_I = v_{II}(t_{II})$ . From Eq. (25), we note that the absolute velocity of the system at switchings is monotonically increasing without bound. The phase portrait depicted in Fig. 2(b) actually corresponds to the free response with  $x(0) = 0$  and  $\dot{x}(0) = v_I = 0$ . The unbounded growth of the solution at switchings, can easily be seen in the figure.

Next we consider the case  $A > 0$ . For a detailed analysis of the forced response, it is convenient to introduce a Poincaré map [25, 31] and study this discrete map instead of the continuous evolution of the system. In the next Section, we compute the switching times that will be needed for obtaining the Poincaré map.

## 5 Switching times

In order to find the switching time  $t_I$  at which transition takes place between subsystems  $I$  and  $II$ , the switching criterion  $x_I(t_I) = 1$  is substituted into Eq. (8) resulting in

$$\frac{1}{2}t_I^2 + \left(v_I - \frac{A}{\omega} \sin(\phi_I)\right)t_I + \frac{A}{\omega^2} \cos(\phi_I) - \frac{A}{\omega^2} \cos(\omega t_I + \phi_I) - 1 = 0. \quad (26)$$

The switching time  $t_I$  is the first positive root of Eq. (26) and is a function of  $v_I$  and  $\phi_I$  for fixed  $A$  and  $\omega$ . Due to the transcendental nature of the equation numerical solution is required (details of the numerical algorithm is provided in the Appendix A. It will be shown that when  $A \leq 1$ , the algorithm works irrespective of the value of  $\omega$ ). The function  $t_I(v_I, \phi_I)$  can have discontinuities corresponding to grazing bifurcations [52, 53] depending on the parameters  $A$  and  $\omega$  (this is discussed in detail in Appendix B). The velocity at the transition (from Eq. (9)) is

$$\dot{x}_I(t_I) = t_I + v_I - \frac{A}{\omega} \sin(\phi_I) + \frac{A}{\omega} \sin(\omega t_I + \phi_I). \quad (27)$$

The phase of the forcing at the transition is simply

$$\phi_I + \omega t_I \bmod 2\pi. \quad (28)$$

Similarly, to find the time  $t_{II}$  of the transition from subsystem  $II$  to subsystem  $I$ , the switching criterion  $x_{II}(t_{II}) = 0$  is substituted into equation Eq. (10) to yield

$$-\frac{1}{2}t_{II}^2 + \left(v_{II} - \frac{A}{\omega} \sin(\phi_{II})\right)t_{II} + \frac{A}{\omega^2} \cos(\phi_{II}) - \frac{A}{\omega^2} \cos(\omega t_{II} + \phi_{II}) + 1 = 0. \quad (29)$$

The switching time  $t_{II}$  is the smallest positive root of this equation. The velocity at the transition is (from Eq. (11))

$$\dot{x}_{II}(t_{II}) = -t_{II} + v_{II} - \frac{A}{\omega} \sin(\phi_{II}) + \frac{A}{\omega} \sin(\omega t_{II} + \phi_{II}) \quad (30)$$

and the phase is  $\phi_{II} + \omega t_{II} \bmod 2\pi$ . From here on, the modulo  $2\pi$  notation for the phase variable will not be explicitly written out.

Next, we outline the procedure for obtaining the discrete Poincaré map.

## 6 Poincaré map

With the knowledge of the switching times, we are now in the position to construct a map to effectively study the behavior of solutions of Eq. (1). First, consider the mapping  $(\dot{x}_I(0) = v_I, \phi_I) \rightarrow (\dot{x}_I(t_I), \phi_I + \omega t_I)$  of the initial velocity and phase to the velocity and phase at the time of the transition from subsystem  $I$  to subsystem  $II$ . Recall that the initial and final positions are uniquely specified by  $x_I(0) = 0$  and  $x_I(t_I) = 1$ . As already mentioned in Section 4, the final velocity and phase for the solution of subsystem  $I$  at the transition (Eqs. (27) and (28)) will serve as initial velocity and phase for the solution of subsystem  $II$ , i.e.

$$v_{II} = \dot{x}_I(t_I) = t_I + v_I - \frac{A}{\omega} \sin(\phi_I) + \frac{A}{\omega} \sin(\phi_{II}), \quad (31)$$

$$\phi_{II} = \phi_I + \omega t_I. \quad (32)$$

Similarly, the final values of velocity and phase of the solution of subsystem  $II$  will provide the initial conditions for the solution of subsystem  $I$  as

$$v_I = \dot{x}_{II}(t_{II}) = -t_{II} + v_{II} - \frac{A}{\omega} \sin(\phi_{II}) + \frac{A}{\omega} \sin(\phi_I), \quad (33)$$

$$\phi_I = \phi_{II} + \omega t_{II}. \quad (34)$$

Rearranging Eqs. (31) and (33) yields

$$v_{II} - \frac{A}{\omega} \sin(\phi_{II}) = t_I + v_I - \frac{A}{\omega} \sin(\phi_I), \quad (35)$$

$$v_I - \frac{A}{\omega} \sin(\phi_I) = -t_{II} + v_{II} - \frac{A}{\omega} \sin(\phi_{II}). \quad (36)$$

The form of these expressions motivates the introduction of a new variable  $z = v - \frac{A}{\omega} \sin(\phi)$ <sup>1</sup>. Equations (35) and (36) can now be rewritten as

$$z_{II} = t_I + z_I, \quad (37)$$

$$z_I = -t_{II} + z_{II}, \quad (38)$$

where  $z_I = v_I - \frac{A}{\omega} \sin(\phi_I)$  and  $z_{II} = v_{II} - \frac{A}{\omega} \sin(\phi_{II})$ . We can now relate initial values of the variables  $z, \phi$  to their values at the switchings by the two maps  $\Pi_I, \Pi_{II}$  as

$$\begin{pmatrix} z_{II} \\ \phi_{II} \end{pmatrix} = \Pi_I \begin{pmatrix} z_I \\ \phi_I \end{pmatrix} = \begin{pmatrix} z_I + t_I \\ \phi_I + \omega t_I \end{pmatrix}. \quad (39)$$

$$\begin{pmatrix} z_I \\ \phi_I \end{pmatrix} = \Pi_{II} \begin{pmatrix} z_{II} \\ \phi_{II} \end{pmatrix} = \begin{pmatrix} z_{II} - t_{II} \\ \phi_{II} + \omega t_{II} \end{pmatrix}. \quad (40)$$

Note that Eq. (40) can also be written as

$$\Pi_{II} \begin{pmatrix} z_{II} \\ \phi_{II} \end{pmatrix} = \begin{pmatrix} z_{II} - t_{II} \\ \phi_{II} + \omega t_{II} \end{pmatrix} = \Psi \circ \Pi_I \circ \Psi \begin{pmatrix} z_{II} \\ \phi_{II} \end{pmatrix}, \quad (41)$$

where  $\Psi$  is the shift map introduced in Eq. (14). To specify the range and domain of these maps, we introduce the Poincaré surfaces  $\Sigma_I = \{(z_I, \phi_I) | x(t) = 0\}$  and  $\Sigma_{II} = \{(z_{II}, \phi_{II}) | x(t) = 1\}$ . Clearly,  $\Pi_I$  and  $\Pi_{II}$  are maps from  $\Sigma_I$  onto  $\Sigma_{II}$  and from  $\Sigma_{II}$  onto  $\Sigma_I$ , respectively. The Poincaré map (a.k.a. return map)  $\Pi$  is now defined

<sup>1</sup>  $z$  is the velocity component induced by the hysteretic force field  $F[x(t)]$ . It can also be viewed as the relative velocity between the solution trajectories of Eq. (1) with  $F[x(t)]$  as defined in Eq. (2) with  $F[x(t)] \equiv 0$ .

as the map of the plane  $\Sigma_I$  onto itself after a pair of switchings. The map  $\Pi$  is therefore obtained by composing the two maps  $\Pi_{II}$  and  $\Pi_I$  as

$$\Pi \begin{pmatrix} z_I \\ \phi_I \end{pmatrix} = \Pi_{II} \circ \Pi_I \begin{pmatrix} z_I \\ \phi_I \end{pmatrix} = \Psi \circ \Pi_I \circ \Psi \circ \Pi_I \begin{pmatrix} z_I \\ \phi_I \end{pmatrix}, \quad (42)$$

where the last equality comes from Eq. (41). The final expression for the Poincaré map in Eq. (42) again emphasizes the symmetry in the problem. Substituting Eqs. (39) and (40) for  $\Pi_I$  and  $\Pi_{II}$  into Eq. (42) results in

$$\Pi \begin{pmatrix} z_I \\ \phi_I \end{pmatrix} = \begin{pmatrix} z_I + t_I(z_I, \phi_I) - t_{II}(z_I, \phi_I) \\ \phi_I + \omega t_I(z_I, \phi_I) + \omega t_{II}(z_I, \phi_I) \end{pmatrix}. \quad (43)$$

Equation (43) defines the Poincaré map  $\Pi$  to be used in the subsequent analysis. The implicit dependence of the switching times  $t_I$  and  $t_{II}$  on  $(z_I, \phi_I)$  is also emphasized. With the new variables  $z_I$  and  $z_{II}$  introduced in Eqs. (26) and (29), the switching times  $t_I$  and  $t_{II}$  are determined as the first positive roots of

$$\frac{1}{2}t_I^2 + z_I t_I + \frac{A}{\omega^2} \cos(\phi_I) - \frac{A}{\omega^2} \cos(\omega t_I + \phi_I) - 1 = 0, \quad (44)$$

$$-\frac{1}{2}t_{II}^2 + z_{II} t_{II} + \frac{A}{\omega^2} \cos(\phi_{II}) - \frac{A}{\omega^2} \cos(\omega t_{II} + \phi_{II}) + 1 = 0, \quad (45)$$

respectively. Substituting for  $z_{II}$  and  $\phi_{II}$  from Eqs. (37) and (32) into Eq. (45) results in

$$-\frac{1}{2}t_{II}^2 + (z_I + t_I)t_{II} + \frac{A}{\omega^2} \cos(\phi_I + \omega t_I) - \frac{A}{\omega^2} \cos(\phi_I + \omega t_I + \omega t_{II}) + 1 = 0. \quad (46)$$

Equations (44) and (46) now define the implicit dependence of  $t_I$  and  $t_{II}$  on  $(z_I, \phi_I)$ . As mentioned previously, the switching times are not necessarily continuous functions of the parameters and depending on the parameters  $A$  and  $\omega$ , the switching times  $t_I$  and  $t_{II}$  can in general have discontinuities corresponding to grazing bifurcations [52, 53] as  $z_I$  and  $\phi_I$  are varied. This will result a discontinuous Poincaré map leading to further complexity of the system. However, in this work, we only consider parameter values  $A$  and  $\omega$  for which the switching times and consequently the Poincaré map are continuous (Appendix B discusses conditions for which this parametric continuity holds).

With the introduction of the Poincaré map we have reduced the study of the original hybrid system (1) to that of the discrete map  $\Pi : \Sigma_I \rightarrow \Sigma_{II}$ . After having obtained the Poincaré map, we now wish to calculate its inverse, to be utilized later for discussing global dynamics of the system.

## 7 Inverse Poincaré map

The Poincaré map was defined as the return map from the surface  $\Sigma_I$  to itself after a pair of switchings and is described by

$$\Pi \begin{pmatrix} z_I \\ \phi_I \end{pmatrix} = \Pi_{II} \circ \Pi_I \begin{pmatrix} z_I \\ \phi_I \end{pmatrix},$$

where  $\Pi_I$  is the map from the surface  $\Sigma_I$  to  $\Sigma_{II}$  while  $\Pi_{II}$  is the map from the surface  $\Sigma_{II}$  to  $\Sigma_I$ . The inverse Poincaré map is given by

$$\Pi^{-1} \begin{pmatrix} z_I \\ \phi_I \end{pmatrix} = \Pi_I^{-1} \circ \Pi_{II}^{-1} \begin{pmatrix} z_I \\ \phi_I \end{pmatrix}. \quad (47)$$

Hence, the map  $\Pi$  is invertible iff the individual maps  $\Pi_I$  and  $\Pi_{II}$  are invertible. We will assume that the individual maps  $\Pi_I$  and  $\Pi_{II}$  are invertible and hence, the maps  $\Pi_I^{-1}$  and  $\Pi_{II}^{-1}$  are uniquely defined. The domain and range of the map  $\Pi_I^{-1}$  are the switching surfaces  $\Sigma_{II}$  and  $\Sigma_I$ , respectively, while the domain and the range of the map  $\Pi_{II}^{-1}$  are the switching surfaces  $\Sigma_I$  and  $\Sigma_{II}$ , respectively. The inverse map will be used in Section 9 to compute backward iterations.

The inverse Poincaré map  $\Pi^{-1}$  is given by the transformation  $t \rightarrow t_I + t_{II} - t$ . Further, the above transformation implies the transformations  $(z_I, \phi_I) \rightarrow (-z_I, -\phi_I)$  and  $(z_{II}, \phi_{II}) \rightarrow (-z_{II}, -\phi_{II})$  for the variables  $z$  and  $\phi$  on the switching surfaces. Thus, using these two transformations, one can compute the individual inverse maps  $\Pi_{II}^{-1}$  and  $\Pi_I^{-1}$  and following (47), take their composition to obtain the inverse Poincaré map. However, a more

straightforward derivation results if one resorts to the equivalent transformation  $t \rightarrow t_I + t_{II} - t$ . In view of this transformation, from (43), it follows that (dropping the modulo  $2\pi$  notation for the phase variable as before)

$$\Pi^{-1} \begin{pmatrix} z_I \\ \phi_I \end{pmatrix} = \Pi_I^{-1} \circ \Pi_{II}^{-1} \begin{pmatrix} z_I \\ \phi_I \end{pmatrix} = \begin{pmatrix} z_I - t_I + t_{II} \\ \phi_I - \omega t_I - \omega t_{II} \end{pmatrix}, \quad (48)$$

where  $t_I$  and  $t_{II}$  are the corresponding switching times to be determined.

To determine switching times  $t_I$  and  $t_{II}$  for this case, we first recall that the domain of  $\Pi_{II}^{-1}$  is  $\Sigma_I$ . Accordingly, the initial conditions for the subsystem  $II$  for the inverse map are  $x_{II}(0) = 0$ ,  $\dot{x}_{II}(0) = -z_I - \frac{A}{\omega} \sin(\phi_I)$ . With these initial conditions, the solution for the subsystem  $II$  is

$$\begin{aligned} x_{II}(t) &= -\frac{1}{2} t^2 - z_I t + \frac{A}{\omega^2} \cos(-\phi_I) - \frac{A}{\omega^2} \cos(\omega t - \phi_I), \\ \dot{x}_{II}(t) &= -t - z_I + \frac{A}{\omega} \sin(\omega t - \phi_I). \end{aligned}$$

Hence, the switching time  $t_{II}$  from the subsystem  $II$  to the subsystem  $I$  using the switching criterion  $x_{II}(t) = 1$  is the root of the equation

$$-\frac{1}{2} t_{II}^2 - z_I t_{II} + \frac{A}{\omega^2} \cos(-\phi_I) - \frac{A}{\omega^2} \cos(\omega t_{II} - \phi_I) - 1 = 0$$

which can be rewritten as

$$\frac{1}{2} t_{II}^2 + z_I t_{II} - \frac{A}{\omega^2} \cos(-\phi_I) + \frac{A}{\omega^2} \cos(\omega t_{II} - \phi_I) + 1 = 0. \quad (49)$$

At the instant of switching from subsystem  $II$  to subsystem  $I$ , we have  $\dot{x}_{II} \leq 0$ . The first root of Eq. (49) is associated with  $\dot{x}_{II} \geq 0$  and therefore, the switching time  $t_{II}$  is the first root of Eq. (49) if  $\dot{x}_{II}(t_{II}) = 0$ , otherwise it is the second root of Eq. (49).

Similarly the initial conditions for the subsystem  $I$  for the inverse map are  $x_I(0) = 1$ ,  $\dot{x}_I(0) = -z_{II} - \frac{A}{\omega} \sin(\phi_{II})$ . With these initial conditions, the solution for the subsystem  $I$  is

$$\begin{aligned} x_I(t) &= 1 + \frac{1}{2} t^2 - z_{II} t + \frac{A}{\omega^2} \cos(-\phi_{II}) - \frac{A}{\omega^2} \cos(\omega t - \phi_{II}), \\ \dot{x}_I(t) &= t - z_{II} + \frac{A}{\omega} \sin(\omega t - \phi_{II}). \end{aligned}$$

Using the above solution along with the switching criterion  $x_I(t) = 0$  results in

$$1 + \frac{1}{2} t_I^2 - z_{II} t_I + \frac{A}{\omega^2} \cos(-\phi_{II}) - \frac{A}{\omega^2} \cos(\omega t_I - \phi_{II}) = 0 \quad (50)$$

which yields the switching time  $t_I$  from the subsystem  $I$  to subsystem  $II$  as its second root.

The switching times  $t_I$  and  $t_{II}$  thus obtained as the second roots of Eqs. (49) and (50) respectively, need to be substituted in (48) to complete the derivation of the inverse Poincaré map. In the following section, we proceed to study the periodic solutions of the system.

## 8 Periodic solutions

We first locate period-one solutions of Eq. (1), i.e., solutions which involve a single pair of switchings between  $\Sigma_I$  and  $\Sigma_{II}$ . Equivalently, we are looking for the fixed points of the Poincaré map  $\Pi$ .

### 8.1 Period-one solutions

Fixed points of the Poincaré map are given by

$$\begin{pmatrix} z_I^* \\ \phi_I^* \end{pmatrix} = \Pi \begin{pmatrix} z_I^* \\ \phi_I^* \end{pmatrix}.$$



Accordingly, Eq. (43) yields the conditions

$$z_I^* = z_I^* + t_I - t_{II}, \quad (51)$$

$$\phi_I^* = \phi_I^* + \omega t_I + \omega t_{II}. \quad (52)$$

Equation (51) gives

$$t_I = t_{II}, \quad (53)$$

which after substitution into Eq. (52) results in

$$t_I = t_{II} = \frac{n\pi}{\omega}, \quad (54)$$

since  $t > 0$ ,  $n \in \mathbb{Z}^+$ . Having obtained the switching times  $t_I$  and  $t_{II}$  for a fixed point of the Poincaré map, we still need to determine the values of  $z_I^*$  and  $\phi_I^*$ . Using Eqs. (44), (46) and (54), we obtain

$$\frac{n^2\pi^2}{2\omega^2} + z_I^* \frac{n\pi}{\omega} - 1 + \frac{A \cos(\phi_I^*)}{\omega^2} (1 - (-1)^n) = 0 \quad (55)$$

and

$$\frac{n^2\pi^2}{2\omega^2} + z_I^* \frac{n\pi}{\omega} + 1 + \frac{A \cos(\phi_I^*)}{\omega^2} ((-1)^n - 1) = 0. \quad (56)$$

Subtracting Eq. (55) from Eq. (56) yields

$$2 + 2 \frac{A \cos(\phi_I^*)}{\omega^2} ((-1)^n - 1) = 0. \quad (57)$$

Equation (57) can only be solved for odd  $n$  to yield

$$\cos(\phi_I^*) = \frac{\omega^2}{2A}. \quad (58)$$

Recall that  $A > 0$ . Since  $|\cos(\phi_I^*)| \leq 1$ , the condition for existence of a period-one solution is given by

$$\omega^2 \leq 2A. \quad (59)$$

From Eq. (58), the initial phase  $\phi_I^*$  corresponding to the period-one solution is obtained as

$$\phi_I^* = \pm \arccos\left(\frac{\omega^2}{2A}\right). \quad (60)$$

Adding Eqs. (55) and (56), we have

$$\frac{n^2\pi^2}{\omega^2} + 2z_I^* \frac{n\pi}{\omega} = 0$$

which can be solved for  $z_I^*$  to give

$$z_I^* = -\frac{n\pi}{2\omega}, \quad n = 1, 3, 5, \dots \quad (61)$$

The countably many values of  $n$  in Eq. (61) together with the two values of  $\phi_I^*$  given by Eq. (60) define two families of fixed points of the Poincaré map for a given set of parameters  $A$  and  $\omega$  as

$$(z_I^*, \phi_I^*)_{1,2} = \left(-\frac{n\pi}{2\omega}, \pm \arccos\left(\frac{\omega^2}{2A}\right)\right), \quad n = 1, 3, 5, \dots \quad (62)$$

Each of these fixed points corresponds to a period-one solution of Eq. (1). The  $x(t)$ - $\dot{x}(t)$  portraits of the system corresponding to  $n = 1, 3, 5$  and  $7$  are shown in Fig. 4. These different period-one motions represent  $1 : n$  subharmonic resonances of the system and they coexist for a given set of parameter values. The period-one solutions shown in Fig. 4 corresponding to  $(-\pi/2, \pi/3)$ ,  $(-\pi/2, -\pi/3)$ ,  $(-3\pi/2, \pi/3)$  and  $(-3\pi/2, -\pi/3)$  are plotted together in Fig. 5 to emphasize their coexistence. The initial conditions for each  $x(t)$ - $\dot{x}(t)$  portrait has been chosen to be consistent with the fixed points given in Eq. (62), i.e., for  $A = 1$ ,  $\omega = 1$  and  $n = 1$ , the initial conditions corresponding to  $z_I = -\pi/2$  and  $\phi_I = -\pi/3$  are  $x(0) = 0$  and  $\dot{x}(0) = -\pi/2 - \sqrt{3}/2$ .

Having obtained the conditions for the existence of period-one solutions of the system governed by Eq. (1), or equivalently the fixed points of the Poincaré map Eq. (43), we perform stability analysis of these fixed points in the next section.

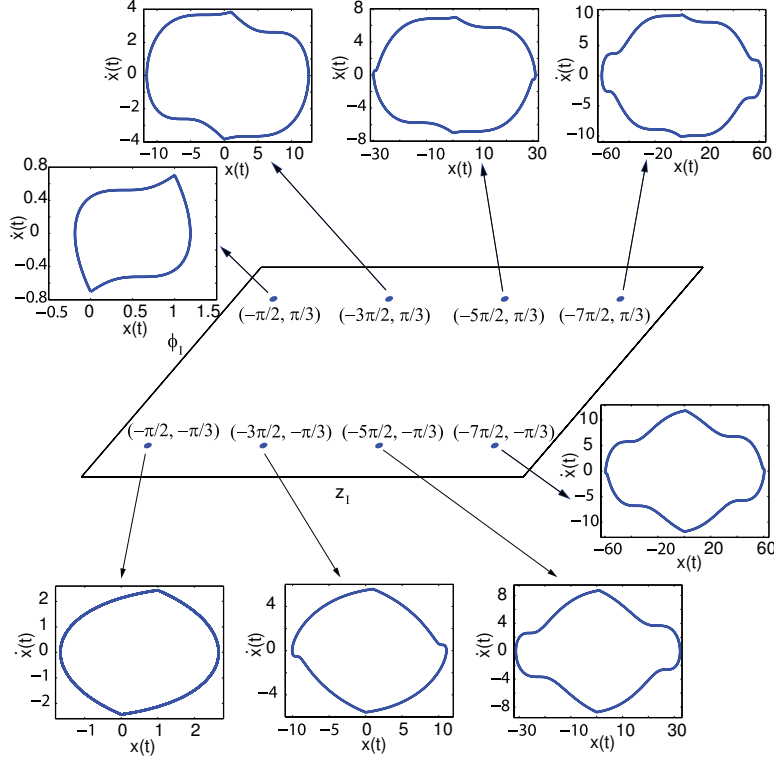


Figure 4:  $x(t)$ - $\dot{x}(t)$  portraits for  $A = 1$  and  $\omega = 1$  corresponding to the fixed points of the Poincaré map for  $n = 1, 3, 5$  and  $7$ .

## 8.2 Stability analysis of period-one solutions

For the purpose of stability analysis of the fixed points of the Poincaré map Eq. (43), we calculate the linearized Poincaré map about the fixed points  $(z_I^*, \phi_I^*)$  using a perturbation expansion. The linearized Poincaré map  $D\Pi$  of map (43) can be written as

$$D\Pi = \begin{pmatrix} 1 + \frac{\partial t_I}{\partial z_I} - \frac{\partial t_{II}}{\partial z_I} & \frac{\partial t_I}{\partial \phi_I} - \frac{\partial t_{II}}{\partial \phi_I} \\ \omega \left( \frac{\partial t_I}{\partial z_I} + \frac{\partial t_{II}}{\partial z_I} \right) & 1 + \omega \left( \frac{\partial t_I}{\partial \phi_I} + \frac{\partial t_{II}}{\partial \phi_I} \right) \end{pmatrix}. \quad (63)$$

The derivatives  $\frac{\partial t_I}{\partial z_I}$ ,  $\frac{\partial t_I}{\partial \phi_I}$ ,  $\frac{\partial t_{II}}{\partial z_I}$  and  $\frac{\partial t_{II}}{\partial \phi_I}$  are obtained by differentiating Eqs. (44) and (46) w.r.t. the variables  $z_I$  and  $\phi_I$ . For example

$$\frac{\partial t_I}{\partial z_I} = -\frac{\omega t_I}{\omega (z_I + t_I) + A \sin(\omega t_I + \phi_I)},$$

$$\frac{\partial t_I}{\partial \phi_I} = \frac{A (\sin(\phi_I) - \sin(\omega t_I + \phi_I))}{\omega (\omega (z_I + t_I) + A \sin(\omega t_I + \phi_I))}.$$

The expressions for  $\frac{\partial t_{II}}{\partial z_I}$  and  $\frac{\partial t_{II}}{\partial \phi_I}$  are a bit lengthier. However, when evaluated at the fixed points, these expressions can be simplified (with the introduction of new variables  $p, q, r$  and  $s$ ) as follows

$$\frac{\partial t_I}{\partial z_I} \Big|_{(z_I^*, \phi_I^*)} = \frac{n \pi}{A \sin(\phi_I^*) - \omega z_I^* - n \pi} = p \quad (64)$$

and

$$\frac{\partial t_I}{\partial \phi_I} \Big|_{(z_I^*, \phi_I^*)} = \frac{2 A \sin(\phi_I^*)}{\omega (A \sin(\phi_I^*) - \omega z_I^* - n \pi)} = q. \quad (65)$$

$$\frac{\partial t_{II}}{\partial z_I} \Big|_{(z_I^*, \phi_I^*)} = \frac{n \pi (\omega z_I^* - 3 A \sin(\phi_I^*))}{(A \sin(\phi_I^*) + \omega z_I^*) (A \sin(\phi_I^*) - \omega z_I^* - n \pi)} = r \quad (66)$$

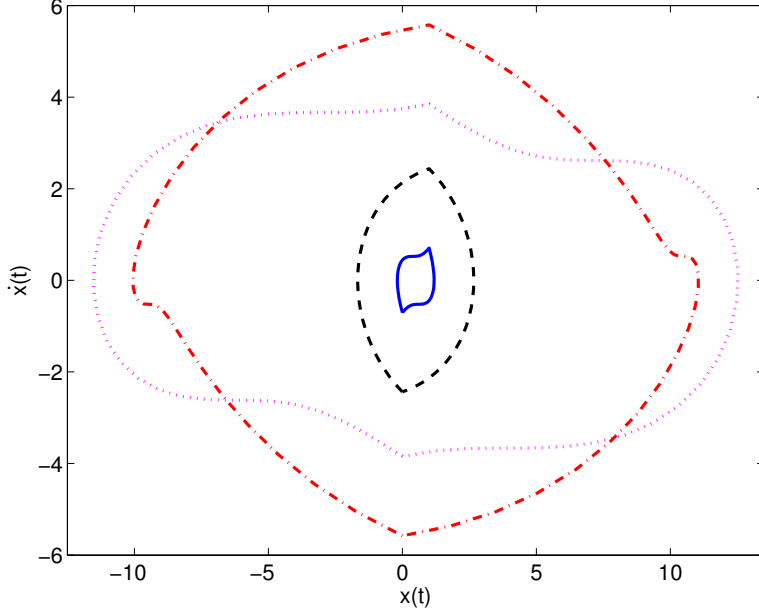


Figure 5:  $x(t)$ - $\dot{x}(t)$  portraits for  $A = 1$  and  $\omega = 1$  corresponding to the fixed points  $(-\pi/2, \pi/3)$  (solid line),  $(-\pi/2, -\pi/3)$  (dashed line),  $(-3\pi/2, \pi/3)$  (dotted line) and  $(-3\pi/2, -\pi/3)$  (dash-dotted line).

and

$$\left. \frac{\partial t_{II}}{\partial \phi_I} \right|_{(z_I^*, \phi_I^*)} = \frac{2A \sin(\phi_I^*) (\omega z_I^* + A \sin(\phi_I^*) + 2n\pi)}{\omega (A \sin(\phi_I^*) + \omega Z_I^*) (A \sin(\phi_I^*) - \omega z_I^* - n\pi)} = s. \quad (67)$$

Now the linearized Poincaré map ( $D\Pi$ ) governing the evolution of the perturbations around the fixed point  $(z_I^*, \phi_I^*)$  can be represented succinctly as

$$D\Pi = \begin{pmatrix} 1 + p - r & q - s \\ \omega(p + r) & 1 + \omega(q + s) \end{pmatrix}. \quad (68)$$

The eigenvalues of the matrix  $D\Pi$  determine the stability of the fixed points of the Poincaré map Eq. (43) or equivalently the period-one solutions of the system Eq. (1). The eigenvalues of  $D\Pi$  are given by

$$\lambda_{1,2} = -\frac{\text{tr}(D\Pi)}{2} \pm \frac{\sqrt{\text{tr}(D\Pi)^2 - 4 \det(D\Pi)}}{2}, \quad (69)$$

where

$$\text{tr}(D\Pi) = 2 + p - r + \omega(q + s)$$

and

$$\det(D\Pi) = 1 + p - r + \omega(2ps + 2qr + q + s).$$

Substituting for  $p$ ,  $q$ ,  $r$  and  $s$  from (64)-(67) in the above, it is easy to verify that  $\det(D\Pi) = 1$  and

$$\text{tr}(D\Pi) = \frac{2(2A \sin(\phi_I^*) + n\pi)^2 + 16An\pi \sin(\phi_I^*)}{(2A \sin(\phi_I^*) - n\pi)^2}. \quad (70)$$

Since  $\lambda_1 \lambda_2 = \det(D\Pi) = 1$ , there are three possibilities for the eigenvalues:

1. Both  $\lambda_1$  and  $\lambda_2$  are real and distinct. In this case, one has a modulus greater than one (eigenvalue outside the unit circle) and the other smaller than one (eigenvalue inside the unit circle). This fixed point is a saddle.
2.  $\lambda_1$  and  $\lambda_2$  are complex conjugate with  $|\lambda_1| = |\lambda_2| = 1$  (eigenvalues on the unit circle). The fixed point is a center.

3. Either  $\lambda_1 = \lambda_2 = 1$  or  $\lambda_1 = \lambda_2 = -1$ . The fixed point is a non-hyperbolic fixed point and nonlinear analysis is required to determine the behavior of the fixed point.

From Eq. (69), we note that the eigenvalues  $\lambda_{1,2}$  are real and distinct if  $\text{tr}(D\Pi) > 2$ , and they are complex conjugate if  $\text{tr}(D\Pi) < 2$ . Substituting  $\phi_I^* = \arccos\left(\frac{\omega^2}{2A}\right)$  in Eq. (70) gives

$$\text{tr}(D\Pi) = \frac{2(4A^2 - \omega^4 + n^2\pi^2 + 6n\pi\sqrt{4A^2 - \omega^4})}{4A^2 - \omega^4 + n^2\pi^2 - 2n\pi\sqrt{4A^2 - \omega^4}}.$$

Clearly  $\text{tr}(D\Pi) > 2$  for  $\omega < \sqrt{2A}$  and hence, the eigenvalues are real and distinct. Therefore, the family of fixed points corresponding to  $\phi_I^* = \arccos\left(\frac{\omega^2}{2A}\right)$  are saddles. Similarly, a substitution of  $\phi_I^* = -\arccos\left(\frac{\omega^2}{2A}\right)$  results in

$$\text{tr}(D\Pi) = \frac{2(4A^2 - \omega^4 + n^2\pi^2 - 6n\pi\sqrt{4A^2 - \omega^4})}{4A^2 - \omega^4 + n^2\pi^2 + 2n\pi\sqrt{4A^2 - \omega^4}} < 2$$

for  $\omega < \sqrt{2A}$ . Hence, the family of fixed points corresponding to  $\phi_I^* = -\arccos\left(\frac{\omega^2}{2A}\right)$  are centers. These two branches of period-one solutions are shown in Fig. 6.

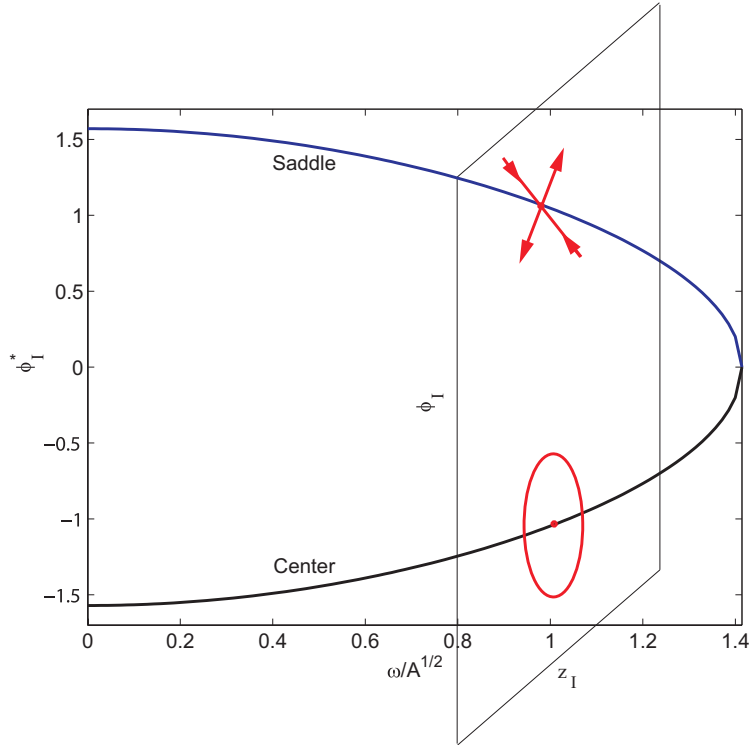


Figure 6: The two branches of fixed points of the Poincaré map Eq. (43).

In the limiting case of  $\omega^2 = 2A$ , the saddle and the center merge in a saddle-center bifurcation [50, 51] leaving a single family of fixed points

$$(z_I^*, \phi_I^*) = \left( \frac{-n\pi}{2\sqrt{2A}}, 0 \right) \quad n = 1, 3, 5, \dots$$

At these points both the eigenvalues are equal to 1. Therefore, this represents a family of non-hyperbolic fixed points.

### 8.3 Higher-period solutions

In this section, we illustrate the procedure for a period-2 solution only. The procedure for higher periodic solutions is similar. A period-2 solution of Eq. (1) is a fixed point of the map  $\Pi^2$ . The sequence of switching times for Eq. (1) are denoted as  $t_I, t_{II}, t_{III}, t_{IV}, \dots$ . Denoting the fixed point of the map  $\Pi^2$  as  $(z_I^{**}, \phi_I^{**})$ , from Eq. (43) we have

$$\begin{pmatrix} z_I^{**} \\ \phi_I^{**} \end{pmatrix} = \Pi \circ \Pi \begin{pmatrix} z_I^{**} \\ \phi_I^{**} \end{pmatrix} = \begin{pmatrix} z_I^{**} + t_I - t_{II} + t_{III} - t_{IV} \\ \phi_I^{**} + \omega(t_I + t_{II} + t_{III} + t_{IV}) \end{pmatrix}$$

From the above, we get two equations, viz.

$$t_I - t_{II} + t_{III} - t_{IV} = 0 \quad (71)$$

and

$$\omega(t_I + t_{II} + t_{III} + t_{IV}) = 2n\pi \quad (72)$$

for some integer  $n$ . We require four more equations in order to be able to solve for the six unknowns  $z_I^{**}, \phi_I^{**}, t_I, t_{II}, t_{III}$  and  $t_{IV}$ . These equations come from the four switching criteria,  $x_I(t_I) = 1, x_{II}(t_{II}) = 0, x_I(t_{III}) = 1$  and  $x_{II}(t_{IV}) = 0$ . Substituting for the appropriate initial conditions in each case, these equations are given by

$$\frac{1}{2}t_I^2 + z_I^{**}t_I + \frac{A}{\omega^2} \cos(\phi_I^{**}) - \frac{A}{\omega^2} \cos(\phi_I^{**} + \omega t_I) - 1 = 0, \quad (73)$$

$$-\frac{1}{2}t_{II}^2 + (z_I^{**} + t_I)t_{II} + \frac{A}{\omega^2} \cos(\phi_I^{**} + \omega t_I) - \frac{A}{\omega^2} \cos(\phi_I^{**} + \omega t_I + \omega t_{II}) + 1 = 0, \quad (74)$$

$$\frac{1}{2}t_{III}^2 + (z_I^{**} + t_I - t_{II})t_{III} + \frac{A}{\omega^2} \cos(\phi_I^{**} + \omega t_I + \omega t_{II}) - \frac{A}{\omega^2} \cos(\phi_I^{**} + \omega t_I + \omega t_{II} + \omega t_{III}) - 1 = 0, \quad (75)$$

$$-\frac{1}{2}t_{IV}^2 + (z_I^{**} + t_I - t_{II} + t_{III})t_{IV} + \frac{A}{\omega^2} \cos(\phi_I^{**} + \omega t_I + \omega t_{II} + \omega t_{III}) - \frac{A}{\omega^2} \cos(\phi_I^{**} + \omega t_I + \omega t_{II} + \omega t_{III} + \omega t_{IV}) + 1 = 0. \quad (76)$$

Equations (71)-(76) need to be solved for the six unknowns  $z_I^{**}, \phi_I^{**}, t_I, t_{II}, t_{III}$  and  $t_{IV}$  numerically. In our simulations, we found no period-2 solutions. However, we found four period-3 solutions which are shown in Fig. 7. These period-3 solutions appear in pairs as noted previously. Solutions  $a$  and  $b$  form a center-type pair, while solutions  $c$  and  $d$  form a saddle-type pair. This is concluded from the numerical evaluation of the eigenvalues of the linearized Poincaré map, i.e., the Floquet multipliers associated with the numerically obtained period-three solution pair. These solution pairs have the symmetry defined by Eqs. (12) and (13) as  $(x_b(t), \dot{x}_b(t)) = (1 - x_a(t), \dot{x}_a(t))$  and  $(x_a(t), \dot{x}_a(t)) = (1 - x_b(t), \dot{x}_b(t))$  where the subscripts  $a$  and  $b$  are used to refer to the solutions  $a$  and  $b$  in Fig. 7. We also found other higher odd period solution pairs and some even period solution pairs. The phase portrait corresponding to the period-8 and period-14 solutions obtained for  $A = 1$  and  $\omega = 1/2$  are shown in Figs. 8 and 9, respectively.

### 8.4 Quasiperiodic solutions

It has been observed numerically that there are invariant curves surrounding the center which correspond to quasiperiodic solutions of Eq. (1). The trajectory of Eq. (1) in the  $x(t)$ - $\dot{x}(t)$  plane corresponding to one of this quasiperiodic solutions for the first few cycles is shown in Fig. 10. A 3D plot corresponding to the quasiperiodic solution shown in Fig. 10 (using a delayed value of the state variable  $x(t)$  as a new variable [54]) is depicted in Fig. 11. The delayed state is used here only for the purpose of illustration. Figure 11 shows that the quasiperiodic solutions lie on a torus. Also plotted in the figure is the period-three solution  $a$  (from Fig. 7 again) to emphasize the coexistence of the quasiperiodic and the period-three solutions.

The winding numbers of these quasiperiodic solutions [45] measure the average rotation induced by the Poincaré map on the Poincaré plane. These prove useful in the classification of the different quasiperiodic solutions, viz., the ones associated with the invariant curves around the center-type period-one solutions and those around the center-type higher periodic solution pairs. To illustrate this, the winding numbers of the quasiperiodic solutions as a function of the distance from the first period-one solution along the  $\phi_I = \phi_I^*$  line are plotted in Fig. 12. The plateaus in Fig. 12 at  $z_I - z_I^* = 0.4$  (0.33) correspond to the period-five (period-three) and associated quasiperiodic solutions around them.

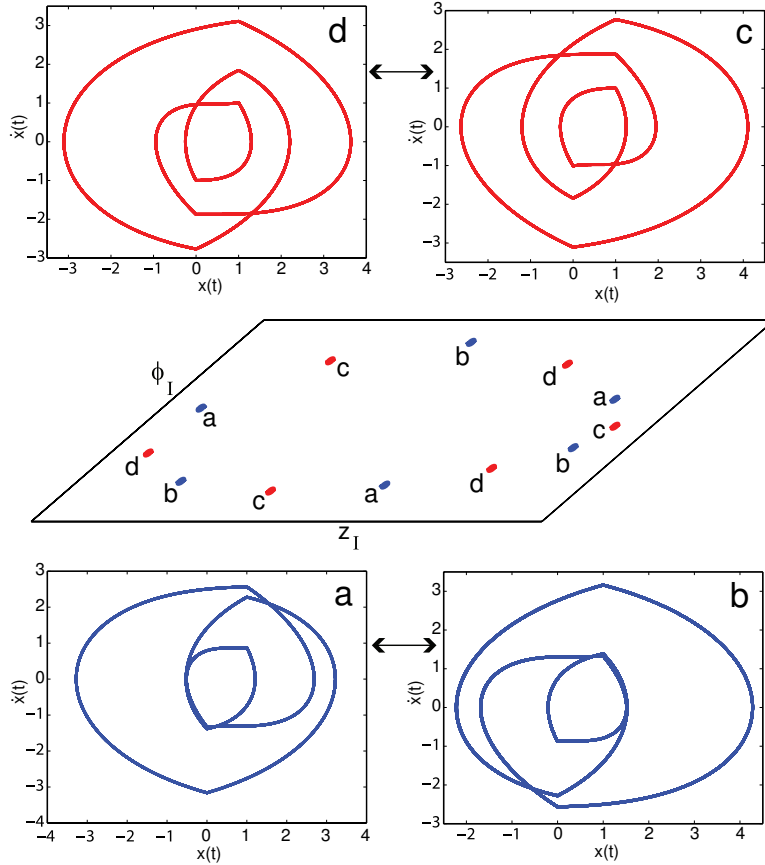


Figure 7:  $x(t)$ - $\dot{x}(t)$  portraits of the period-three solutions of Eq. (1) for  $A = 1$  and  $\omega = 1$ .

## 9 Global dynamics

The presence of centers and saddles on the Poincaré plane hints towards possible homoclinic and heteroclinic orbits or tangles. The dynamics of the system in the  $z$ - $\phi$  variables on the Poincaré plane for  $A = 1$  and  $\omega = 1$  is shown in Fig. 13. Here we have shown the dynamics around the first three centers and saddles. The eigenvector for the first saddle is also plotted in the figure and matches well with the numerically observed directions of the stable and unstable manifolds of the saddle. While it seems that there is a homoclinic orbit around the center, the unstable and the stable manifolds of the saddles intersect transversally giving rise to chaotic tangles. A zoomed view of the boxed portion of Fig. 13 (bottom) is shown in Fig. 13 (top). Here, we notice the presence of isolated invariant curves close to the apparent homoclinic orbit. These isolated curves correspond to quasiperiodic solutions around the center type period-three solution pair. Also shown are the approximate heteroclinic connections between the saddle type period-three solution pair. The presence of several higher period solution pairs hints toward the existence of a Smale horseshoe [31, 55] related to the transverse intersection of the stable and unstable manifolds of the saddle. In Fig. 14, we have plotted the result of forward and backward iterations of  $250 \times 250$  points in a small neighborhood of the saddle. To compute the backward iterations, the inverse Poincaré map presented in Section 7 is used. The transverse intersection of the stable and the unstable manifolds of the saddle is clearly visible in Fig. 14. This numerical evidence shows the existence of a Smale horseshoe which imply the existence of an infinite number of higher periodic and bounded aperiodic solutions.

At the saddle-center bifurcation point, we have a single family of non-hyperbolic fixed points on the Poincaré plane.

## 10 Conclusions

Dynamics of a system with a hysteretic relay operator with simple harmonic forcing is studied in this paper. A Poincaré map has been introduced to facilitate the analysis. Conditions on the amplitude and frequency of the

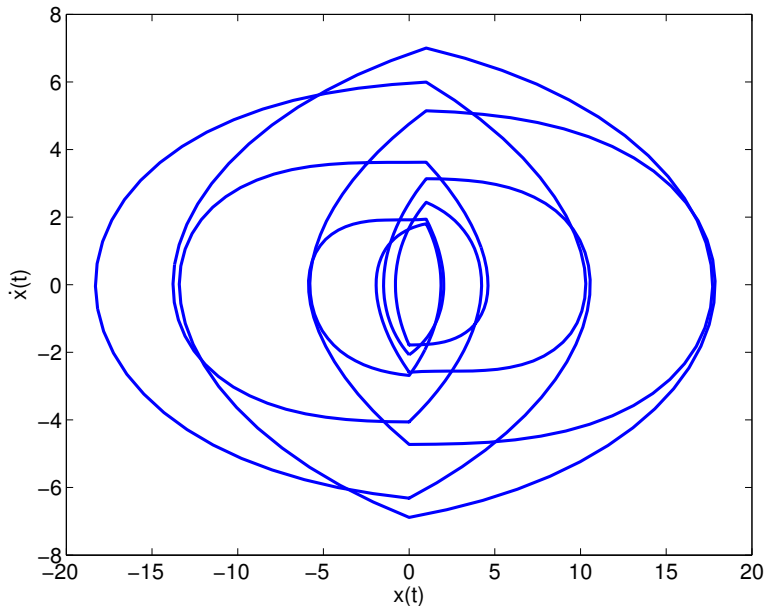


Figure 8:  $x(t)$ - $\dot{x}(t)$  portrait of the period-8 solution of Eq. (1) for  $A = 1$  and  $\omega = 1/2$ . Initial conditions:  $z_I = -0.1328$  and  $\phi_I = -1.3325$

forcing for the existence of periodic solutions have been obtained. There are two families of period-one solutions determined as the fixed points of the Poincaré map. On the Poincaré plane, one family of the fixed points is a center and the other one is a saddle. Higher-period solutions have been obtained numerically. Invariant curves surrounding the center on the Poincaré plane have been obtained which correspond to quasiperiodic solutions. Homoclinic and heteroclinic tangles have been observed numerically implying the presence of chaotic solutions.

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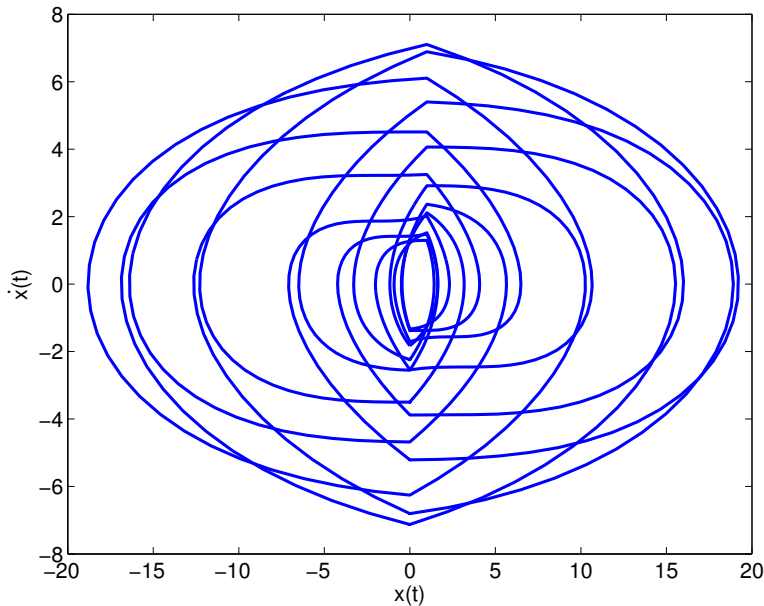


Figure 9:  $x(t)$ - $\dot{x}(t)$  portrait of the period-14 solution of Eq. (1) for  $A = 1$  and  $\omega = 1/2$ . Initial conditions:  $z_I = 0.1067$  and  $\phi_I = -1.3203$

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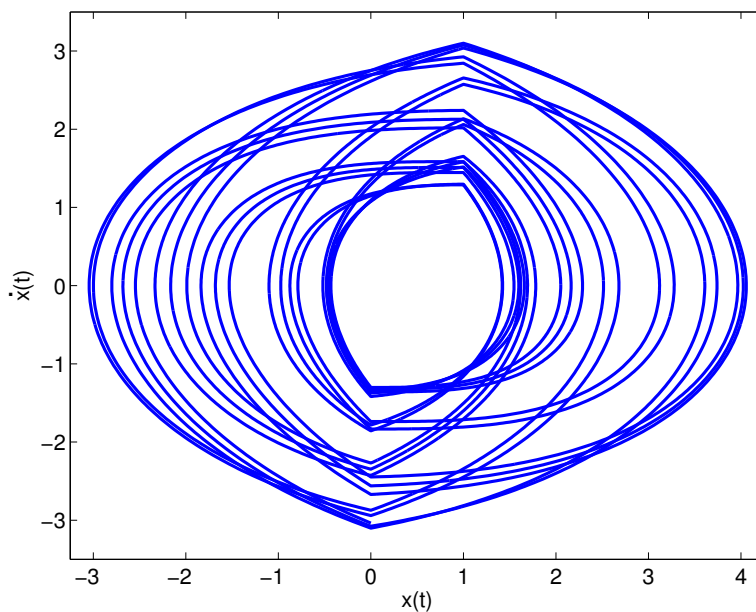


Figure 10:  $x(t)$ - $\dot{x}(t)$  portrait corresponding to a quasiperiodic solution of Eq. (1) for  $A = 1$  and  $\omega = 1$ . Initial conditions correspond to  $z_I = -0.97$  and  $\phi_I = -\pi/3$ , i.e.,  $x(0) = 0$  and  $\dot{x}(0) = -1.83$ .

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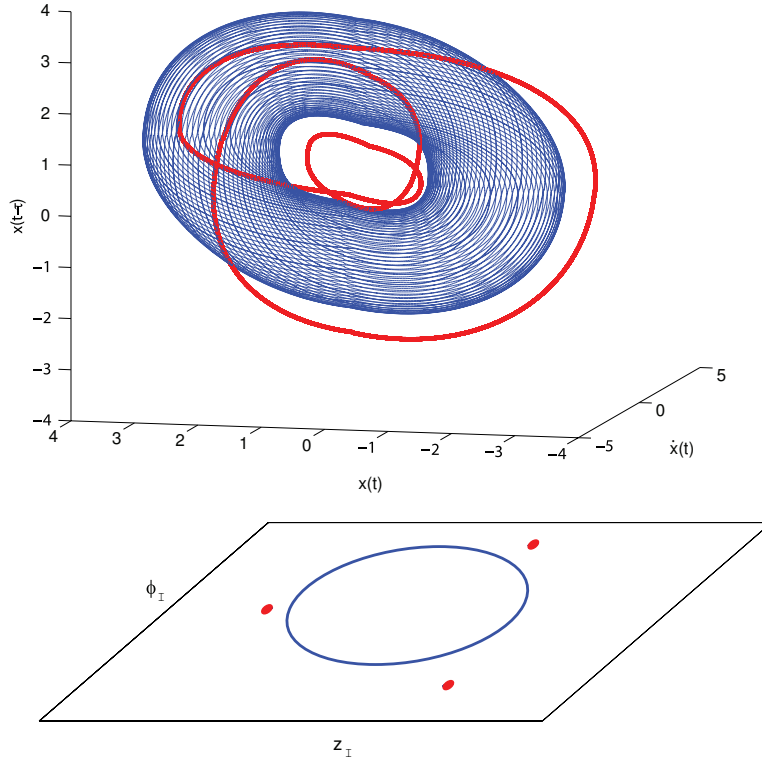


Figure 11: 3D plot in  $x(t)$ - $\dot{x}(t)$ - $x(t - \tau)$  space with  $\tau = \pi/2$  corresponding to Fig. 10. The thick curve represents one of the three-period solutions corresponding to Fig. 7

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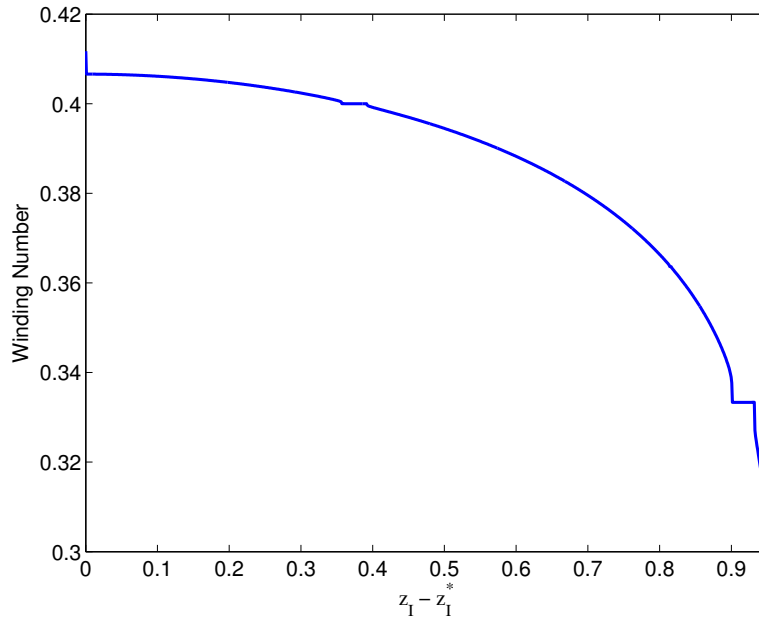


Figure 12: Winding number vs.  $z_I - z_I^*$  for the quasiperiodic solutions of Eq. (1) around the period-one solution corresponding to  $z_I^* = -\pi/2$  and  $\phi_I^* = -\pi/3$  for  $A = 1$  and  $\omega = 1$ .

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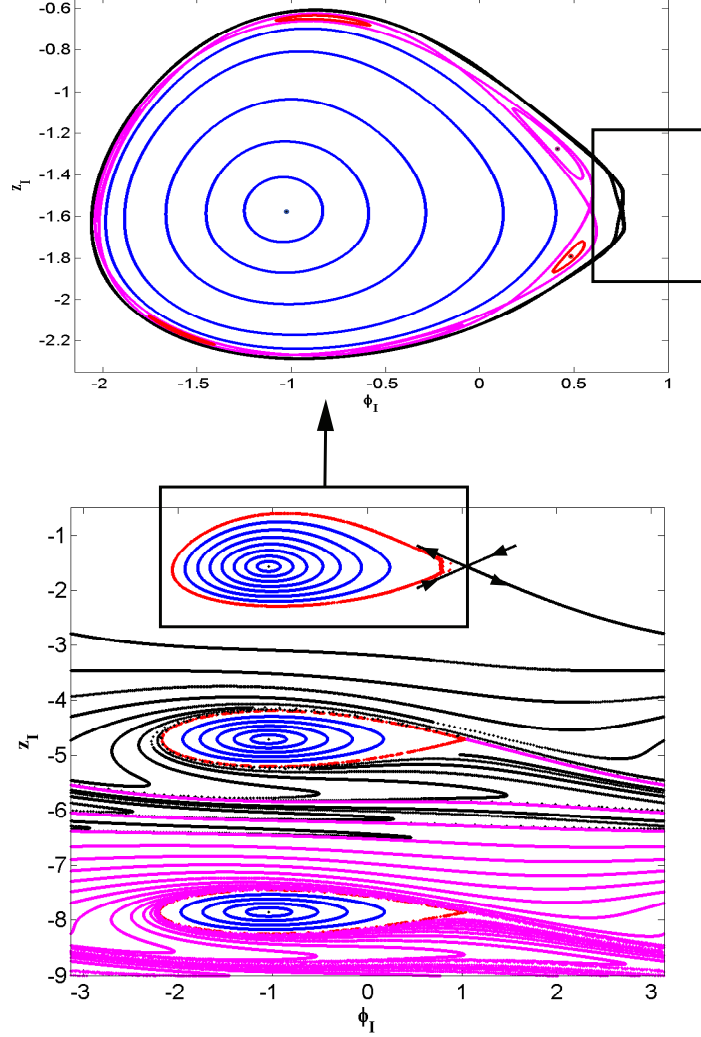


Figure 13: Dynamics around first three centers and saddles in  $\phi_I$ - $z_I$  plane for  $A = 1$  and  $\omega = 1$ .

## A Numerical algorithm to obtain the first positive root of a second order polynomial containing a cosine term

The first positive root of Eqs. (26) and (29) can be obtained by forward marching in time with a suitably chosen time step as in [45]. To obtain the first root with sufficient numerical accuracy, the time step required might be very small when there are two roots close to each other which renders the time-marching algorithm inefficient. This motivates the development of an algorithm wherein we identify disjoint intervals which can contain only a single root and use standard numerical root-finding algorithms like the bisection method in these intervals to locate the roots therein.

The switching conditions, Eqs. (26) and (29), can be written in the general form as

$$a t^2 + b t + c - d \cos(\omega t + \phi) = 0. \quad (77)$$

First we reduce the number of free parameters in Eq. (77) by dividing throughout by  $d$  and scaling time as  $\tau = \omega t$ . This reduces Eq. (77) to

$$a_1 \tau^2 + b_1 \tau + c_1 - \cos(\tau + \phi) = 0, \quad (78)$$

where  $a_1 = \frac{a}{d\omega^2}$ ,  $b_1 = \frac{b}{d\omega}$  and  $c_1 = \frac{c}{d}$ . The first root  $t$  of Eq. (77) is related to the first root  $\tau$  of Eq. (78) as  $t = \frac{\tau}{\omega}$ . The algorithm for reliably obtaining the first root of Eq. (78) can be summarized as follows:

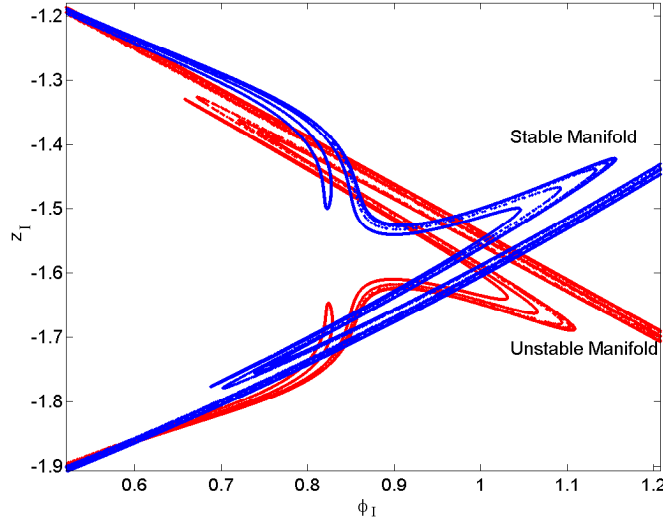


Figure 14: Dynamics in  $\phi_I$ - $z_I$  plane for  $A = 1$  and  $\omega = 1$  showing transverse intersection of the stable and unstable manifolds of the saddle. The region corresponds to the boxed region in Fig. 13 (top).

1. The first step involves identifying the intervals in which the roots of Eq. (78) can possibly exist. To determine these intervals, Eq. (78) is rewritten as  $f(\tau) - g(\tau) = 0$  where  $f(\tau) = a_1 \tau^2 + b_1 \tau + c_1$  and  $g(\tau) = \cos(\tau + \phi)$ . Since  $|g(\tau)| \leq 1$ , feasible intervals for the roots of  $f(\tau) - g(\tau) = 0$  are determined by the roots of  $f(\tau) \pm 1 = 0$ . We define the set of real positive roots of  $f(\tau) \pm 1 = 0$  as  $R = \{r_i \in \mathbb{R}^+ | f(r_i) \pm 1 = 0\}$ . The feasible intervals are now determined by the cardinality of the set  $R$  (denoted by  $n(R)$ ) along with the members of  $R$  as follows. For  $n(R) = 0$ , there are no real positive roots of  $f(\tau) - g(\tau) = 0$ . For  $n(R) > 0$ , the feasible intervals for the roots are given by  $[0, r_1]$  for  $n(R) = 1$ ,  $[r_1, r_2]$  for  $n(R) = 2$ ,  $[0, r_1] \cup [r_2, r_3]$  for  $n(R) = 3$  and  $[r_1, r_2] \cup [r_3, r_4]$  for  $n = 4$ , where  $0 < r_1 < r_2 < r_3 < r_4$ .
2. Each of the feasible intervals for the roots of  $f(\tau) - g(\tau) = 0$  determined in the previous step can have multiple number of roots. The next step in the algorithm, therefore, involves partitioning the above intervals into sub-intervals (not necessarily of equal length) such that each sub-interval can have exactly one root. But this can only happen if the function is monotonic in that sub-interval. To ensure this, we use the fact that a function is monotonic in the interval in which its derivative has the same sign and hence, can have only one root in that interval. This requirement can be met if somehow we can guarantee that our 'target sub-interval' (which we seek to obtain in a way that it contains either zero or exactly one root) contains exactly one inflexion point of the slopes.

Thus, we simply need to compute the zeros of the second derivative of the function and then construct the sub-intervals such that each sub-interval contains exactly one zero of the second derivative, hence exactly one inflexion point of the first derivative and hence the monotonicity, of the function itself, is guaranteed. As a result, now the bisection algorithm can be applied as we already know that the sub-interval on which we are applying bisection, contains at most one root. To perform the above partition, we proceed as follows:

- (a) Since  $f''(\tau) = 2a_1$  and  $g''(\tau) = -\cos(\tau + \phi)$ , the roots of  $f''(\tau) - g''(\tau) = 0$  can be obtained in closed form (for  $|a_1| \leq \frac{1}{2}$ ) as

$$\tau_{dd} = 2m\pi \pm (\arccos(-2a_1) - \phi), \quad m = 0, 1, 2, \dots$$

For  $|a_1| > \frac{1}{2}$ ,  $f''(\tau) - g''(\tau) = 0$  has no real roots. The roots  $\tau_{dd}$  along with the endpoints of the feasible intervals provide a partition of the feasible intervals into feasible sub-intervals such that  $f'(\tau) - g'(\tau) = 0$  can have only one root in each subinterval. It can be noted that all numerical simulations given in this paper accord with the condition  $|a_1| \leq \frac{1}{2}$ , namely forcing amplitude is chosen in a way such that it does not exceed unity.

- (b) The existence of roots of  $f'(\tau) - g'(\tau) = 0$  in the sub-intervals determined in the previous step is ascertained by evaluating  $f'(\tau) - g'(\tau)$  at the endpoints of the subinterval. If the value is zero at either of the end-points, that end-point is the root  $\tau_d$  of  $f'(\tau) - g'(\tau) = 0$ . If the function  $f'(\tau) - g'(\tau)$  changes sign at the end-points, there is a root  $\tau_d$  in the subinterval which can be obtained using the bisection method otherwise there is no root in that sub-interval. The roots  $\tau_d$  of  $f'(\tau) - g'(\tau) = 0$  in each of the subintervals along with the end-points of the feasible intervals form a partition of the feasible intervals into sub-intervals such that  $f(\tau) - g(\tau) = 0$  can have only one root in each subinterval.
3. Having obtained sub-intervals of the semi-real axis  $\mathbb{R}^+$  such that there can be exactly one root of the function  $f(\tau) - g(\tau) = 0$  in each sub-interval, each sub-interval is checked for the roots analogous to the procedure described for the roots of  $f'(\tau) - g'(\tau)$  in the previous step. The procedure starts with the first sub-interval and is terminated if either a root is obtained or all the sub-intervals are exhausted in which case there are no real positive roots of Eq. (78).

## B Grazing discontinuities in the switching times

As mentioned in Appendix A, determination of the switching times require solution of Eqs. (26) and (29) which are of the form of Eq. (77). Geometrically, the roots of the transcendental equation (77) represent points of intersection of a parabola and a cosine curve. Since the parameters  $b$ ,  $c$  and  $\phi$  in the above equation depend on the state variables  $z_I$  and  $\phi_I$ , or  $z_{II}$  and  $\phi_{II}$ , therefore, the switching times  $t_I$  and  $t_{II}$  are functions of the state variables  $z_I$  and  $\phi_I$ , and  $z_{II}$  and  $\phi_{II}$ , respectively. A 3D plot of this function for the first switching time  $t_I(z_I, \phi_I)$  for  $A = 1$  and  $\omega = 1$ , and  $z_I \in [-4, 0]$  and  $\phi_I \in [-\pi, \pi]$  is shown in Fig. 15.

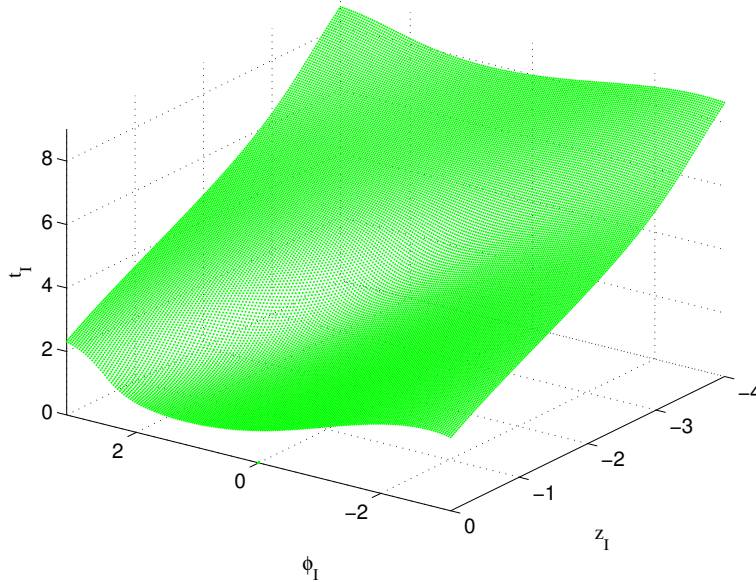


Figure 15: A 3D plot of the function  $t_I(z_I, \phi_I)$  for  $A = 1$  and  $\omega = 1$ .

From Fig. 15, we note that the function defines a smooth surface for these parameter values. However, the function for the switching times can in general have discontinuities corresponding to a grazing intersection of the parabola and the trigonometric function as shown in Fig. 16. The first intersection of the parabola and the trigonometric function is shown by a \*. It can be seen from Fig. 16 that a small change in the parameters result in a large discontinuous change in the first intersection point.

For a grazing intersection, the velocity at the instant of switching  $t_I$  is zero as well. Hence, the equations related to the grazing intersection are given by

$$\frac{1}{2}t_I^2 + z_I t_I + \frac{A}{\omega^2} \cos(\phi_I) - \frac{A}{\omega^2} \cos(\omega t_I + \phi_I) - 1 = 0$$

and

$$t_I + z_I + \frac{A}{\omega} \sin(\omega t_I + \phi_I) = 0.$$

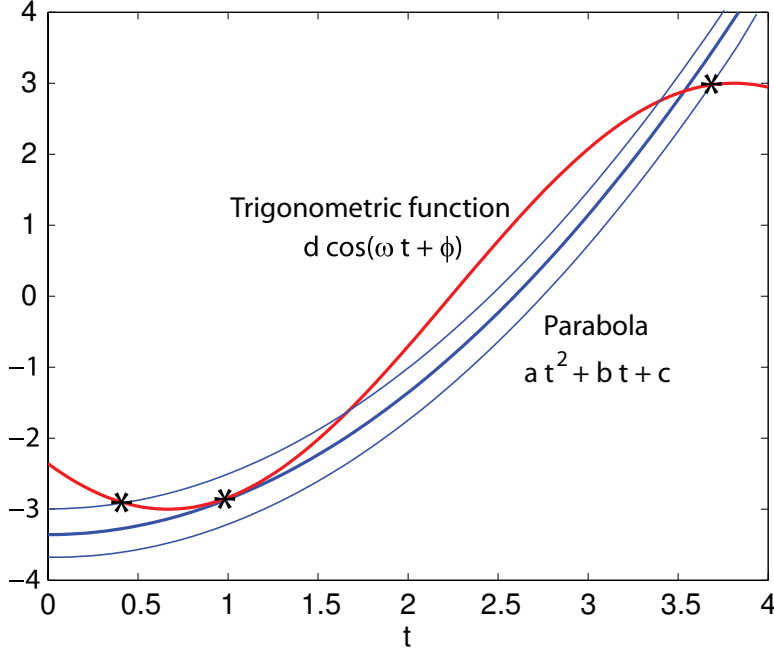


Figure 16: Grazing intersection of a parabola and the cosine curve.

For a given set of parameters  $A$  and  $\omega$ , a point in the plane  $(z_I, \phi_I)$  for which the above set of equations is satisfied for some real positive  $t_I$  is a grazing point. We define the set of all grazing points in the plane  $(z_I, \phi_I)$  as the grazing curve for that particular set of parameters  $A$  and  $\omega$ . From the above set of equations, the switching time  $t_I$  can be solved in closed form in terms of  $z_I$ ,  $\phi_I$ ,  $A$  and  $\omega$  using trigonometric elimination. However, our aim is to get the grazing curves and not necessarily the switching time at grazing. We use a fixed arc-length based continuation scheme (see [?]) in conjunction with the Newton-Raphson method to obtain these grazing curves. The grazing curves for  $A = 3$  and different values of  $\omega$  are plotted in Fig. 17. Thick lines represent the curves of actual discontinuities in  $t_I$  and thin dotted lines represent the case when the grazing root is the second root and hence does not correspond to a discontinuity in  $t_I$ . These two curves form a closed loop in the  $z_I - \phi_I$  plane. A 3D plot of the function  $t_I(z_I, \phi_I)$  for  $A = 3$  and  $\omega = 1$  is shown in Fig. 18 which clearly illustrates the discontinuities in the function  $t_I(z_I, \phi_I)$ . Also plotted with a thick line is the grazing curve. It can be seen that the discontinuities in the function  $t_I(z_I, \phi_I)$  correspond exactly to the grazing curve.

It can be seen from Fig. 17 that the length of the grazing curves decrease with increasing  $\omega$ . In general, there exist a value of  $\omega = \omega_{\text{critical}}$  for which this loop degenerates into a point. For  $\omega > \omega_{\text{critical}}$ , there are no discontinuities in the function  $t_I(z_I, \phi_I)$ . This value of  $\omega_{\text{critical}}$  decreases with a decrease in the other parameter  $A$ . It has been observed numerically that  $\omega_{\text{critical}} \rightarrow 0$  as  $A \rightarrow 1$  from above. This implies that for  $A \leq 1$ , there are no discontinuities in the function  $t_I(z_I, \phi_I)$  for any  $\omega$ . This can be demonstrated as follows:

The acceleration of the subsystem  $I$  is given by

$$\ddot{x}_I(t) = 1 + A \cos(\omega t + \phi).$$

For  $A \leq 1$ ,  $\ddot{x}_I(t) \geq 0$  and hence the velocity of the subsystem is monotonic and non-decreasing. Therefore, the equation  $\dot{x}_I(t) = 0$  can have only one real root. Next, we consider two cases:  $\dot{x}_I(0) \geq 0$  and  $\dot{x}_I(0) < 0$ .

1. For the case of  $\dot{x}_I(0) \geq 0$ ,  $\dot{x}_I(t) > 0$  for  $t > 0$ . Therefore,  $\dot{x}_I(t_I) > 0$  where  $t_I$  is the root of  $x_I(t_I) - 1 = 0$ . Hence, the two equations  $x_I(t) - 1 = 0$  and  $\dot{x}_I(t) = 0$  cannot hold simultaneously. This implies that there can be no grazing intersection and accordingly no discontinuities in the function  $t_I(z_I, \phi_I)$  for any value of  $\omega$ .
2. For the case of  $\dot{x}_I(0) < 0$ , the equation  $x_I(t) = 0$  has a single root say  $t = t_d$ . However, for  $t \in [0, t_d)$ ,  $\dot{x}(t) < 0$  and therefore, the displacement  $x(t)$  is monotonically decreasing in this interval. Since  $x(0) = 0$ , it follows that  $x(t_d) < 0$  and therefore,  $x(t_d) - 1 < 0$ . Again this implies that the two equations  $x_I(t) - 1 = 0$  and  $\dot{x}_I(t) = 0$  cannot hold simultaneously and hence, there can be no discontinuities in the function  $t_I(z_I, \phi_I)$ .

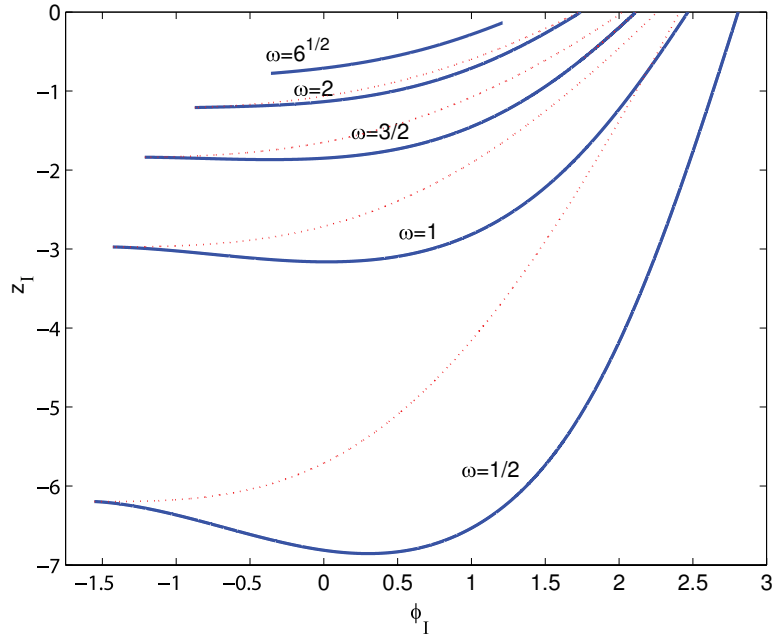


Figure 17: Grazing curves for  $A = 3$ . Thick lines represent the curves of actual discontinuities in  $t_I$  and thin dotted lines represent the case when the grazing root is the second root and hence does not correspond to a discontinuity in  $t_I$ .

Hence, for  $A \leq 1$ , the function  $t_I(z_I, \phi_I)$  is continuous for any value of the parameter  $\omega$ .



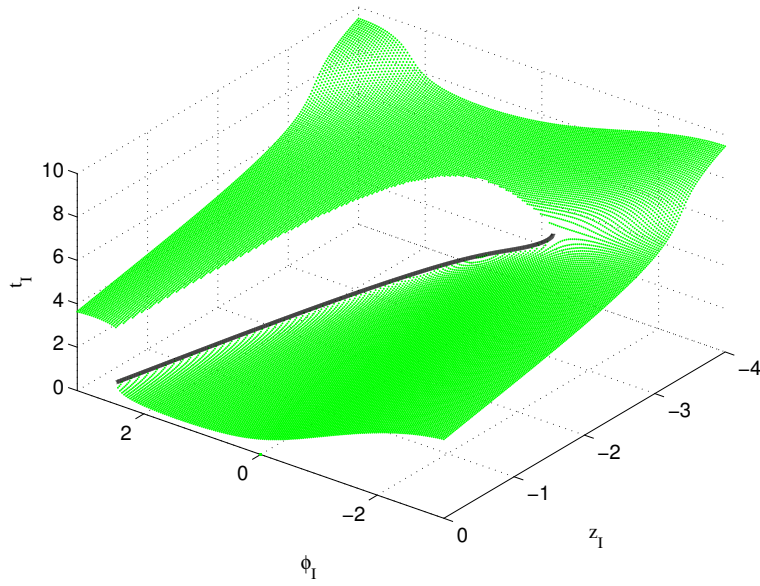


Figure 18: A 3D plot of the function  $t_I(z_I, \phi_I)$  for  $A = 3$  and  $\omega = 1$ .